

# Worldwide Pollution Control Association

WPCA-  
Southern Company  
Mercury Seminar  
October 30-31, 2012

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# SCR and Hg Oxidation



Johnson Matthey  
Catalysts



**WPCA Hg Co-benefits Seminar**  
**Birmingham, AL**  
**October 30-31, 2012**

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ENVIRONMENTAL CATALYSTS AND TECHNOLOGIES



# Agenda



- SCR Catalyst co-benefit
- Hg Oxidation Mechanism
- Effect of different constituents on Hg Oxidation
- Catalyst Management for Mercury Oxidation
- Mercury Oxidation Testing



# Mercury Removal Requirement due to MATS rule



- Existing
  - 1.2 lb/TBTU (0.013 lb/GWh) for Bituminous Coal
  - 11 lb/TBTU (0.12 lb/GWh) for Subbituminous Coal Units
- New
  - 0.0002 lb/GWh for Bituminous Coal
  - 0.04 lb/GWh for Subbituminous Coal
- These limits to be met using a comprehensive AQCS Hg strategy



# SCR and Mercury Oxidation



- Mercury emissions can exist in a variety of forms
  - Total –  $\text{Hg}^T$  includes  $\text{Hg}^0$ ,  $\text{Hg}^{2+}$ ,  $\text{Hg}^P$
  - $\text{Hg}^P$  – Particulate bound mercury
  - $\text{Hg}^0$  – elemental mercury
  - $\text{Hg}^{2+}$  – oxidized mercury
- SCR catalyst has the ability to oxidize elemental mercury
  - Reaction is complex, and dependent on many parameters
- Oxidized mercury
  - Water soluble - able to be captured in wet-FGD
  - Easier to capture by activated carbon than elemental mercury
- Creating oxidized mercury does not guarantee capture

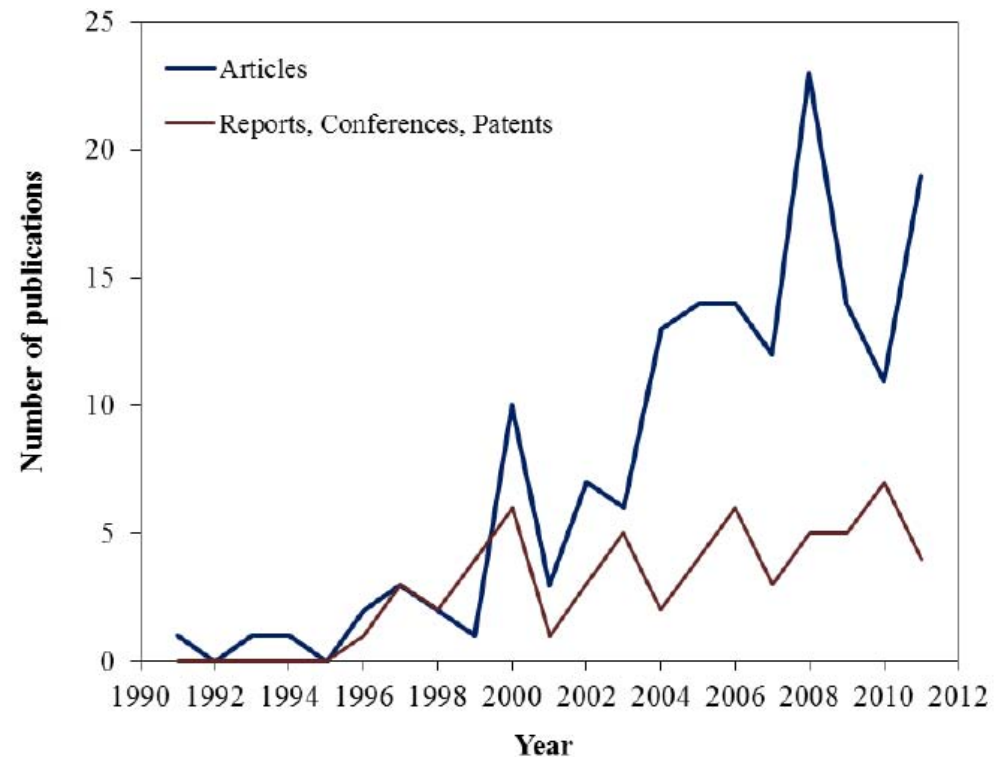


# SCR and Mercury Oxidation



- SCR catalyst and Mercury Oxidation research increasing
  - Increase likely to continue due to MATS final rule and potential co-benefit of SCR
  - Can SCR-FGD configuration be relied on, or do alternate capture schemes need to be installed?

Number of Publications about Hg Oxidation



Source: Dranga et al. (2012)



# Sponsored Oxidation Testing (not a complete list)



- DOE NETL Cooperative Agreement DE-FC26-02NT41589
  - Evaluation of Mercury Emissions from Coal-Fired Facilities with SCR and FGD systems (2006)
- EPA Cooperative Agreement R-829353-01
  - Effect of Selective Catalyst Reduction on Mercury (2004)
- US DOE NETL - Evaluation of the Effect of SCR NOx Control Technology on Mercury Speciation (2003)
- EPRI Report No. 1005400
  - Power Plant Evaluation of the Effect of Selective Catalytic Reduction in Mercury (2002)
- DOE Cooperative Agreement No: DE- FC26-03NT41728
  - Oxidation of Mercury Across SCR Catalyst in Coal Plants Burning Low Rank Coal (2004)
- **These and other studies demonstrate the SCR co-benefit; next step is refining plant operations to ensure consistent and predictable stack Hg emissions**



# Mercury Capture



- Activated Carbon Injection (ACI)
  - Adsorbs both  $\text{Hg}^0$  and  $\text{Hg}^{2+}$ , preferential towards  $\text{Hg}^{2+}$
  - ACI then can be captured in particulate control device
- Novel Sorbent and Non-Carbon additive injection
  - Capture both  $\text{Hg}^0$  and  $\text{Hg}^{2+}$
  - Can be captured in particulate control device
- Wet-FGD
  - Captures mostly  $\text{Hg}^{2+}$
  - Some issues in capture have been found, seem related to ORP
- Unburned carbon show some ability to capture mercury
- Oxidized mercury has potential to reduce back to elemental mercury downstream of SCR



# Reactions of Hg



## Desired Reactions – Hg oxidation

- $\text{Hg} + 2 \text{HCl} + \frac{1}{2} \text{O}_2 \rightarrow \text{HgCl}_2 + \text{H}_2\text{O}$
- $\text{Hg} + \text{SO}_3 + \frac{1}{2} \text{O}_2 \rightarrow \text{HgSO}_4$
- $2 \text{HCl} + \frac{1}{2} \text{O}_2 \rightarrow \text{Cl}_2 + \text{H}_2\text{O}$
- $\text{Hg} + \text{Cl}_2 \rightarrow \text{HgCl}_2$

## Other Reactions

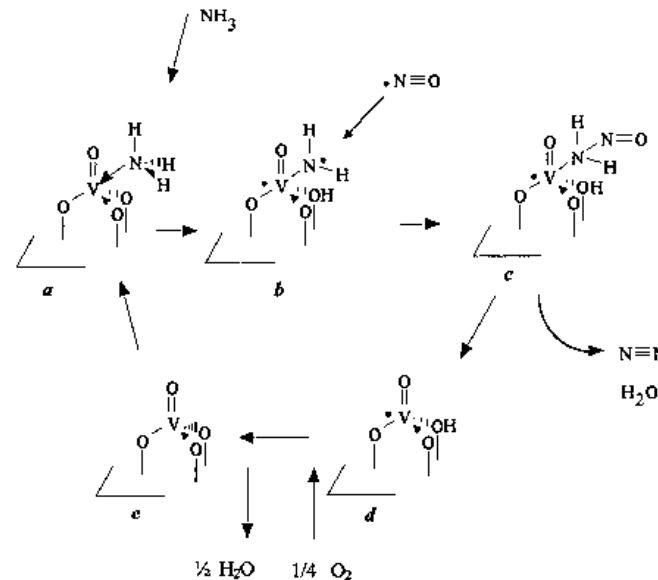
- $\text{Cl}_2 + \text{SO}_2 + \text{H}_2\text{O} \rightarrow 2 \text{HCl} + \text{SO}_3$
- $3 \text{HgCl}_2 + 2 \text{NH}_3 \rightarrow 3 \text{Hg} + 6 \text{HCl} + \text{N}_2$ , reduction of Hg by  $\text{NH}_3$
- $\text{HgCl}_2 + \text{SO}_2 + \text{H}_2\text{O} \rightarrow \text{Hg} + 2 \text{HCl} + \text{SO}_3$ , reduction of Hg by  $\text{SO}_2$



# Potential Mechanism



- There is an industry accepted mechanism of DeNO<sub>x</sub> – Eley Rideal



Source: Lietti et Al. (1998)

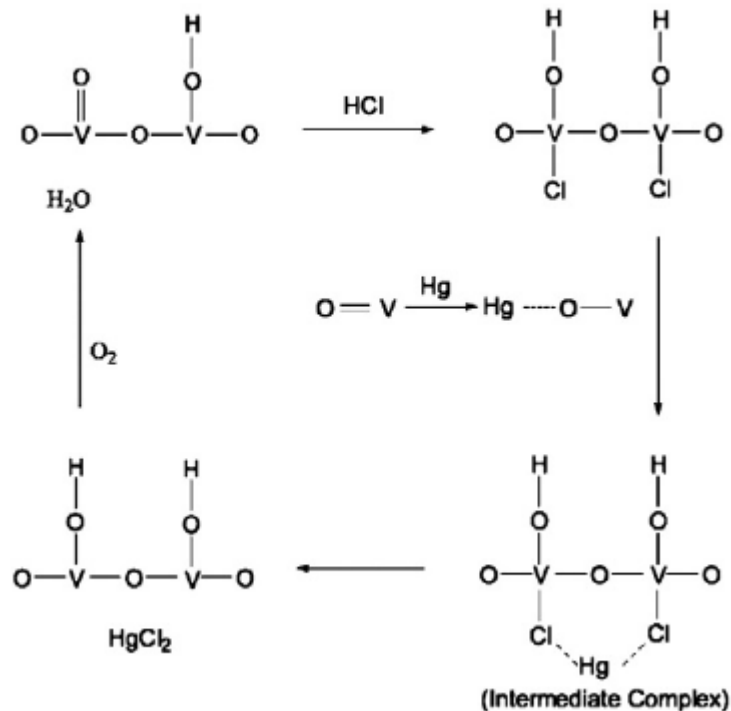
- Speculation on Mercury oxidation mechanism over SCR still exists, but:
  - Hg<sup>0</sup> seems to adsorb, then react
  - HCl reacts from either adsorbed state or gaseous state



# Potential Hg Mechanism



Langmuir Hinshelwood:



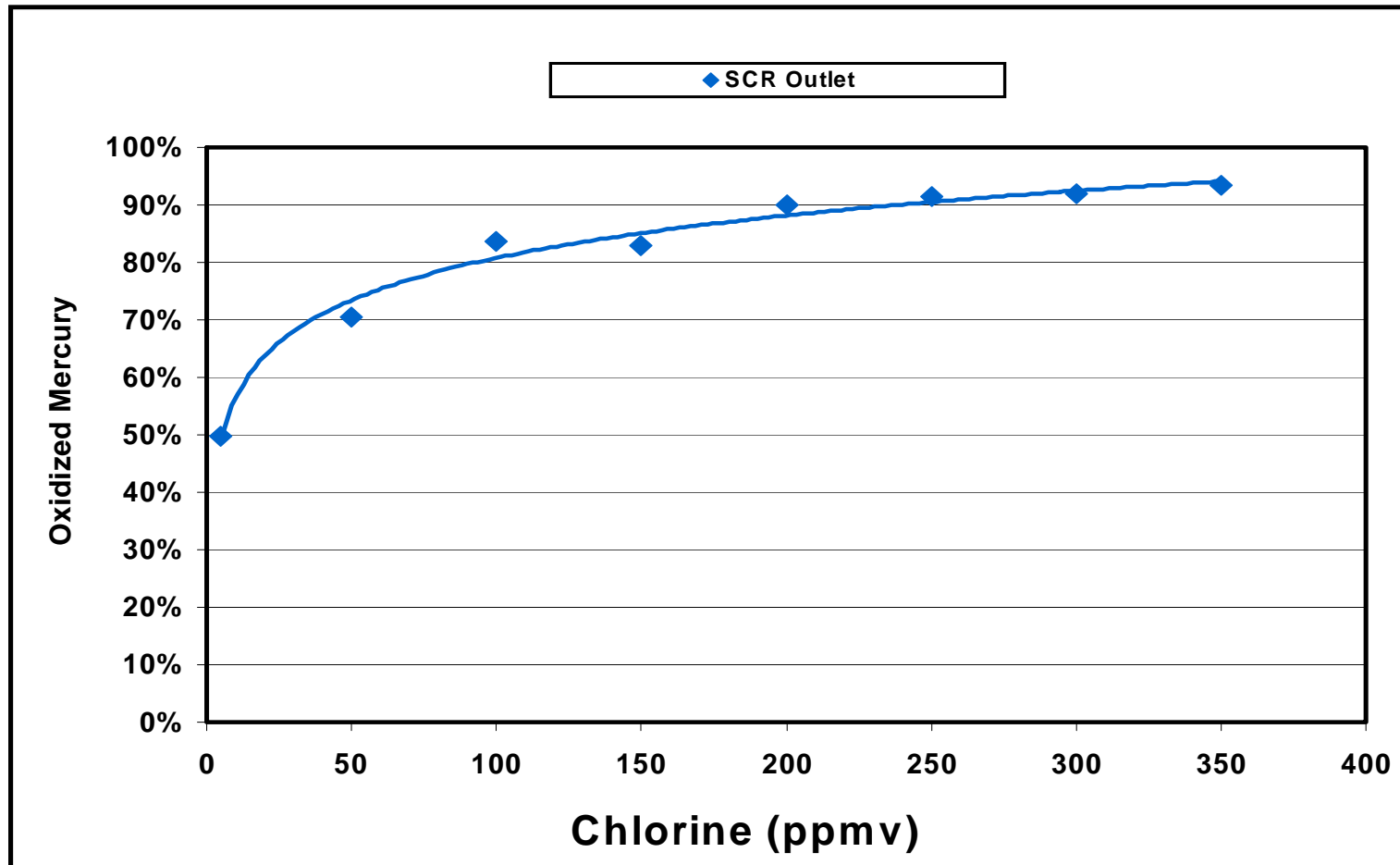
Source: He et al. (2009)

Eley Rideal, HCl does not adsorb:

- Hg adsorbs on vanadium oxide active site, creates a vanadium-mercury-oxide site
- HCl in the gas phase reacts with adsorbed Hg, creating oxidized mercury species
- Product diffuses off catalyst, active site is regenerated



# Hg Oxidation in Catalyst – General Effect of Cl



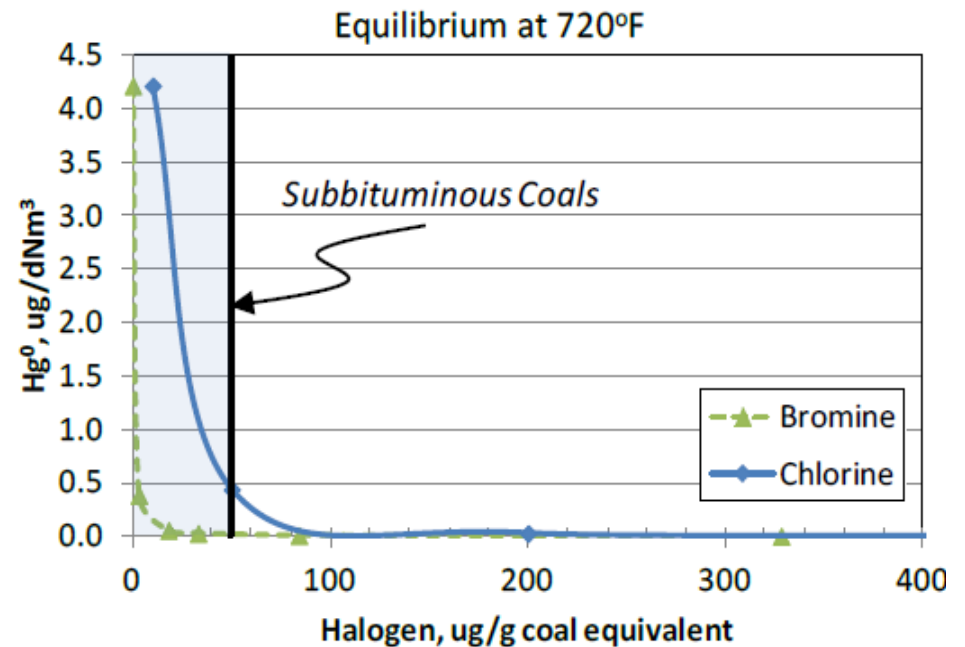
Reproduced by permission from *Effects of Chlorine and other Flue Gas Parameters on SCR Catalyst Mercury Oxidation and Capture*, EPRI, Palo Alto, CA 2009. 1020591



# Key Characteristics of Mercury Oxidation



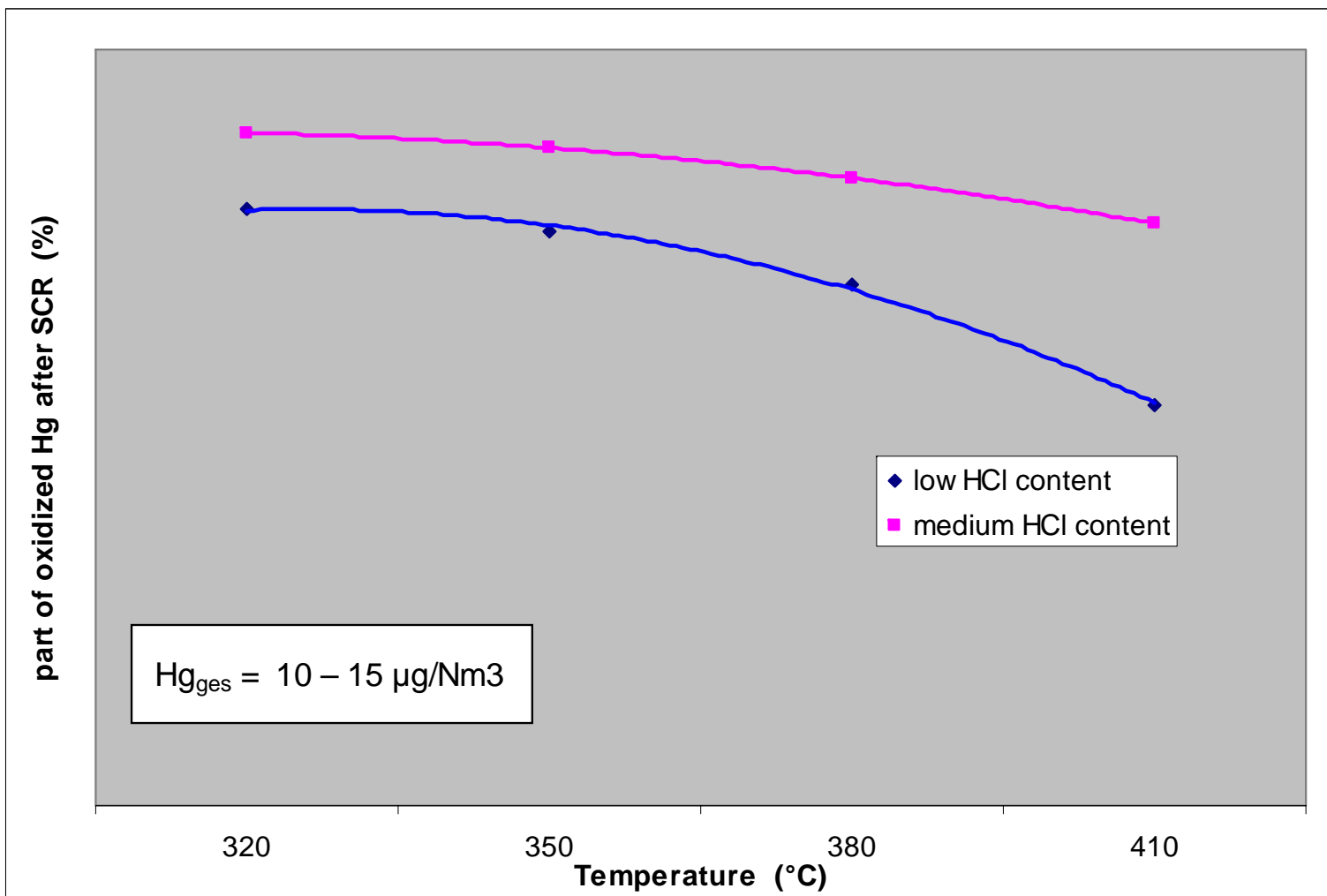
- Bromine is more effective than Chlorine at improving mercury oxidation
- Bromine has been shown to improve heterogeneous (over catalyst) and homogeneous (without catalyst) oxidation of mercury



Source: Senior et al., Berry et al.



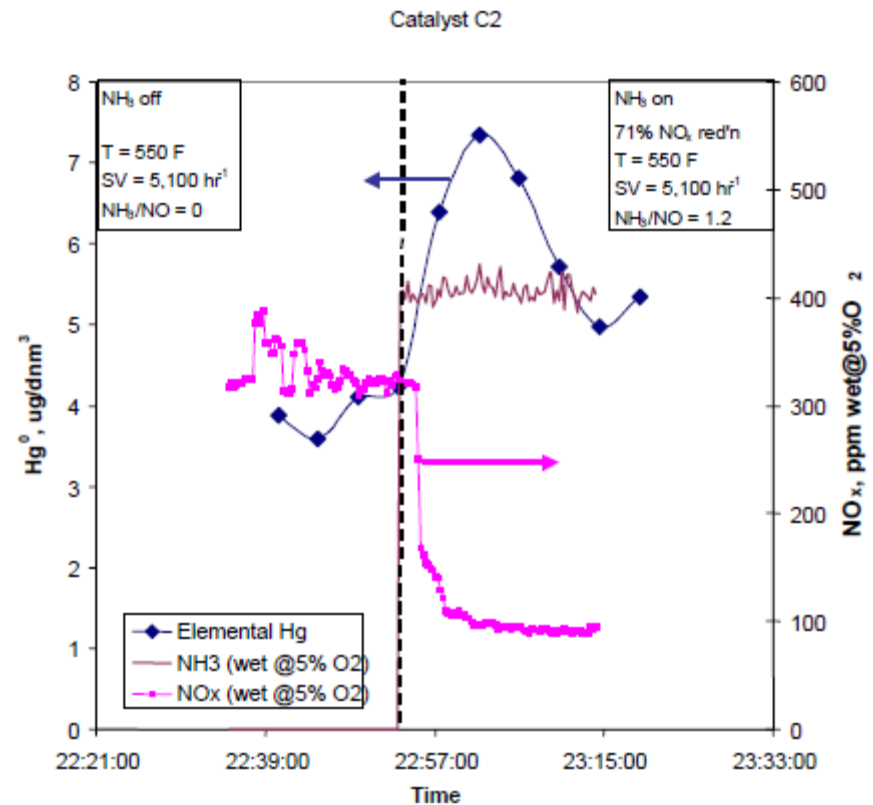
# Hg Oxidation in Catalyst – Effects of Temperature and Cl



# Key Characteristics of Mercury Oxidation



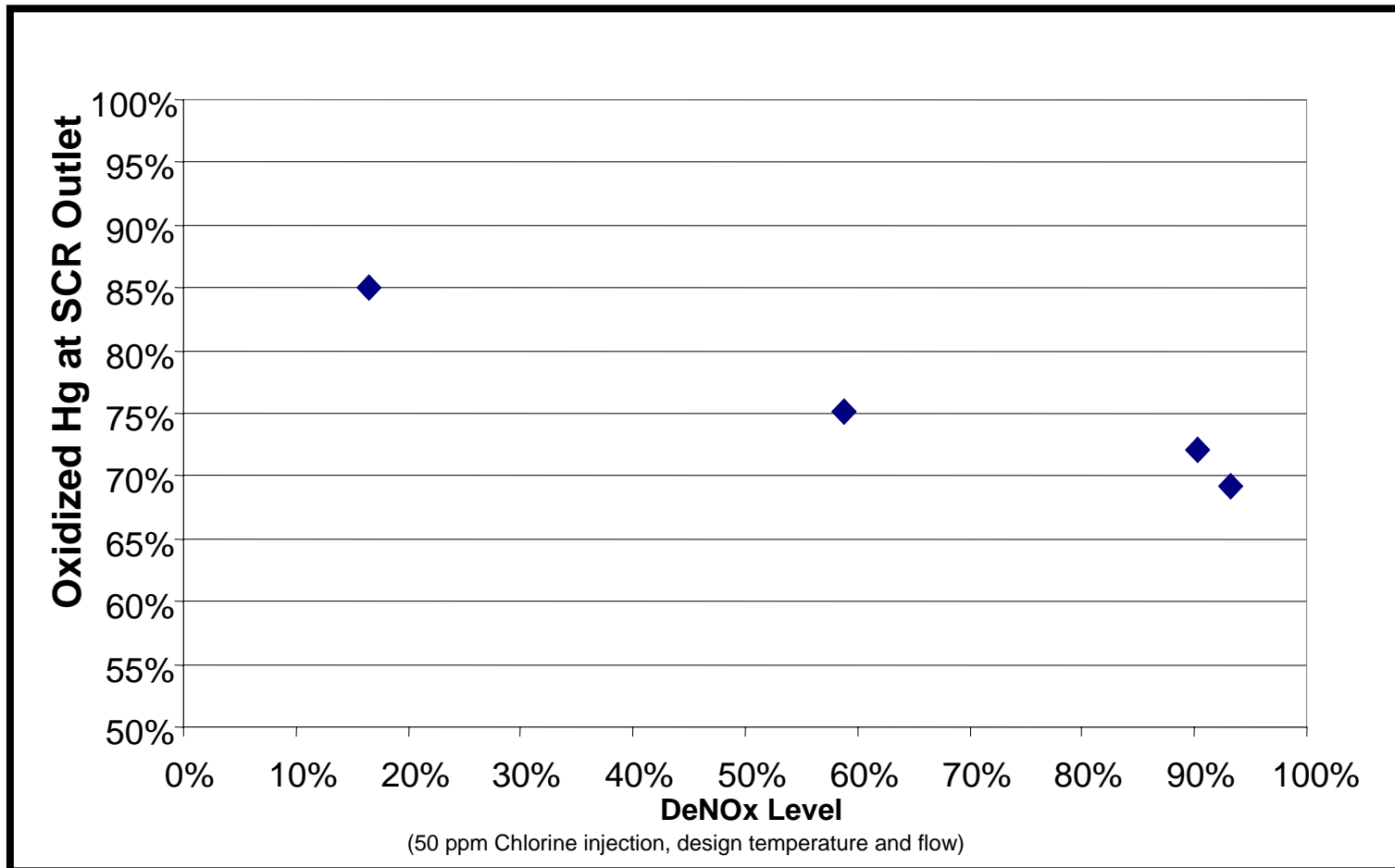
- Ammonia has ability to inhibit mercury adsorption on the catalyst
  - Decreases mercury oxidation when this occurs
  - Reaction not independent with respect to ammonia
  - Some data show that at very high halogen concentrations, mercury oxidation did not decrease to the extent predicted (Hinton 2012)



Source: Senior (2004)



# Hg Oxidation in Catalyst – General Effect of NH<sub>3</sub>



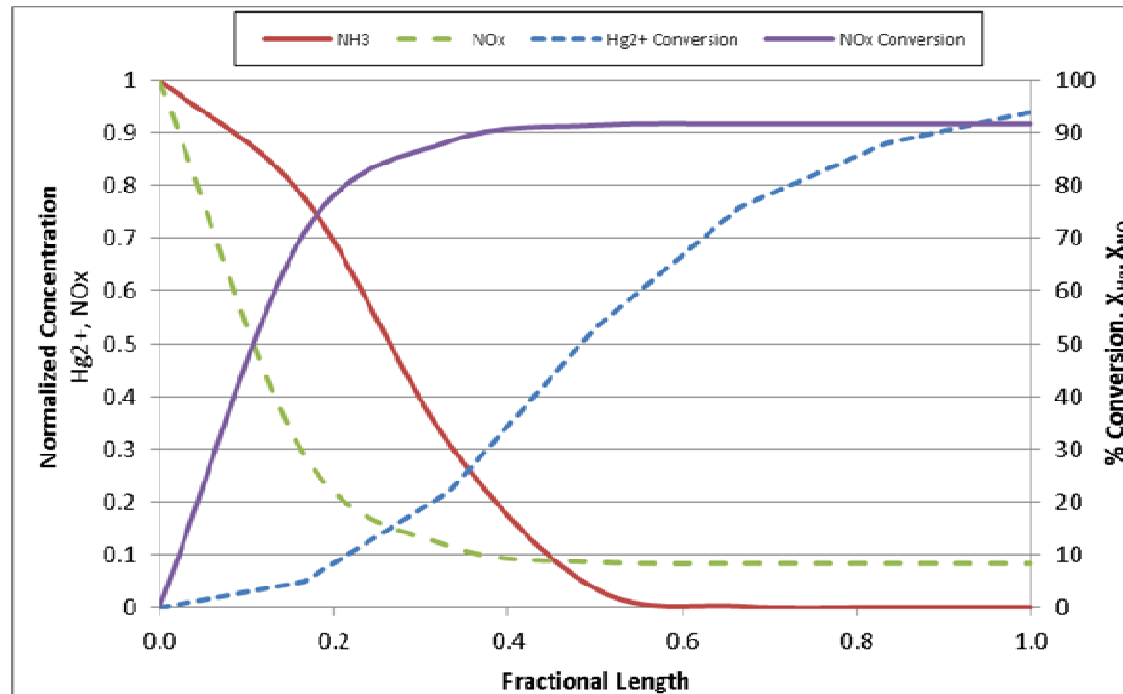
Reproduced by permission from *Effects of Chlorine and other Flue Gas Parameters on SCR Catalyst Mercury Oxidation and Capture*, EPRI, Palo Alto, CA 2009. 1020591



# Key Characteristics of Mercury Oxidation



- As ammonia is consumed within the SCR reactor, the oxidation of mercury increases



# Key Characteristics of Mercury Oxidation



- Other parametric effects (all other parameters constant):
  - Increased Flowrate will decrease mercury oxidation (large impact)
  - Increased O<sub>2</sub> concentration will increase mercury oxidation (medium impact)
  - Increased SO<sub>2</sub> concentration will decrease mercury oxidation (small impact)
  - Increased SO<sub>3</sub> concentration will increase mercury oxidation
- Based on more limited data
  - Increased CO concentration will decrease mercury oxidation (medium impact)
  - Increased H<sub>2</sub>O concentration (medium impact)



# Catalyst Management and Mercury Oxidation

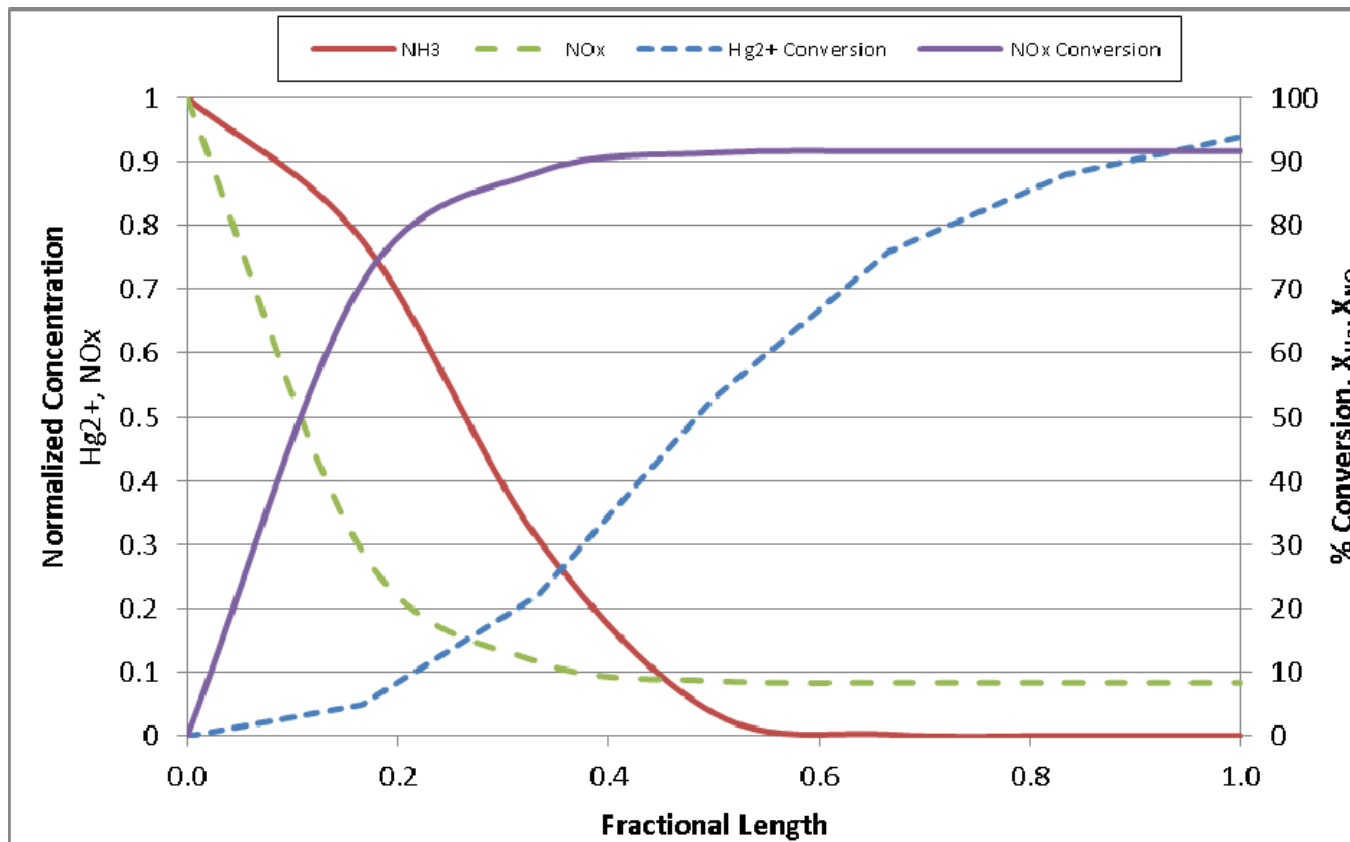


NOx reduction and Hg Oxidation compete

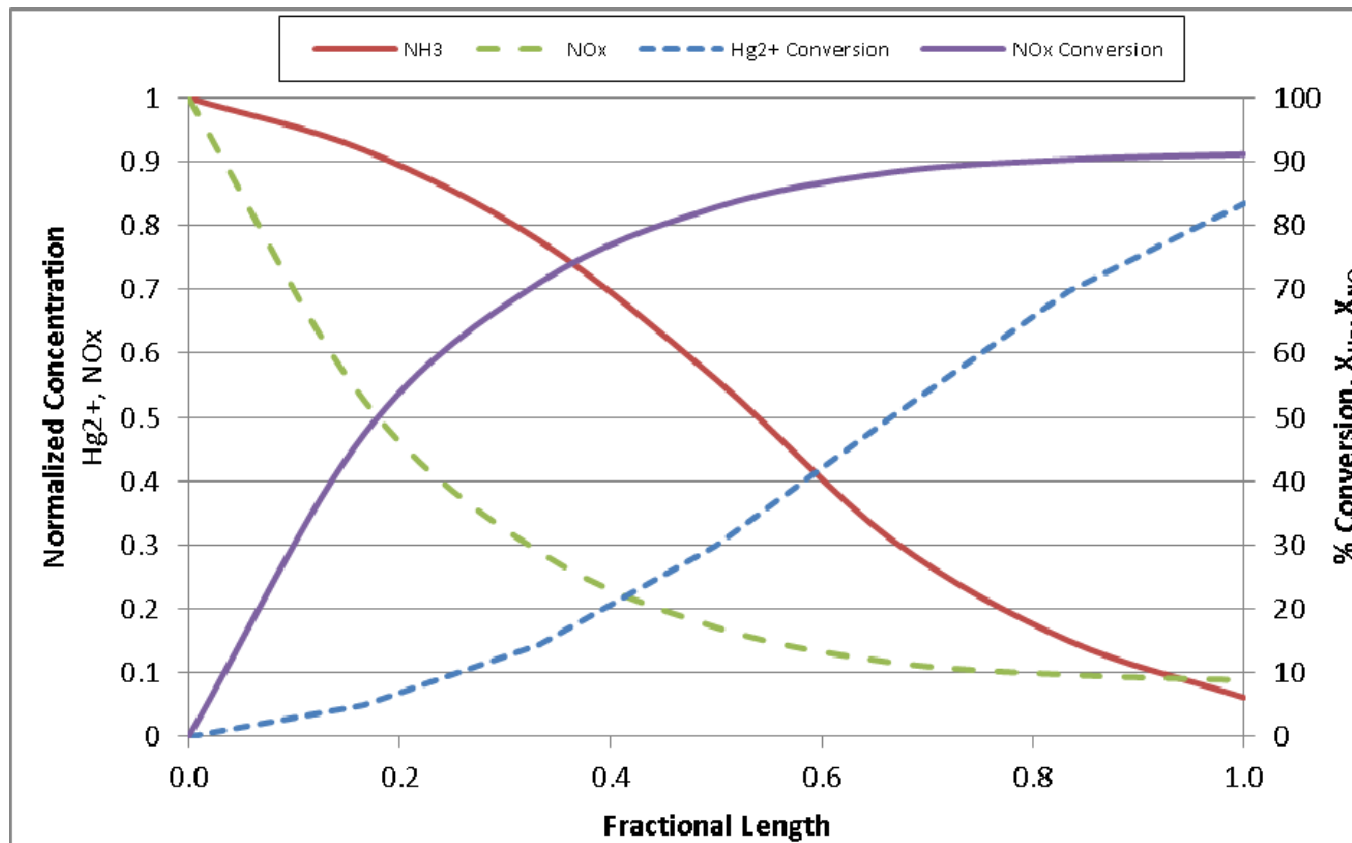
- NOx conversion can be maintained by increasing ammonia flow, allowing plant operators to maintain NOx outlet requirements
- Hg oxidation can be increased by decreasing NOx requirement
- Hg oxidation favored in lower catalyst layers as NH<sub>3</sub> is depleted
- Both can be increased by adding catalyst
  - Trade-offs – SO<sub>2</sub> conversion, pressure drop
- Many plants will start managing catalyst based on mercury oxidation potential



# Effect of Catalyst Aging - New



# Effect of Catalyst Aging - Exposed



# Lab Testing – Predicting Field Performance



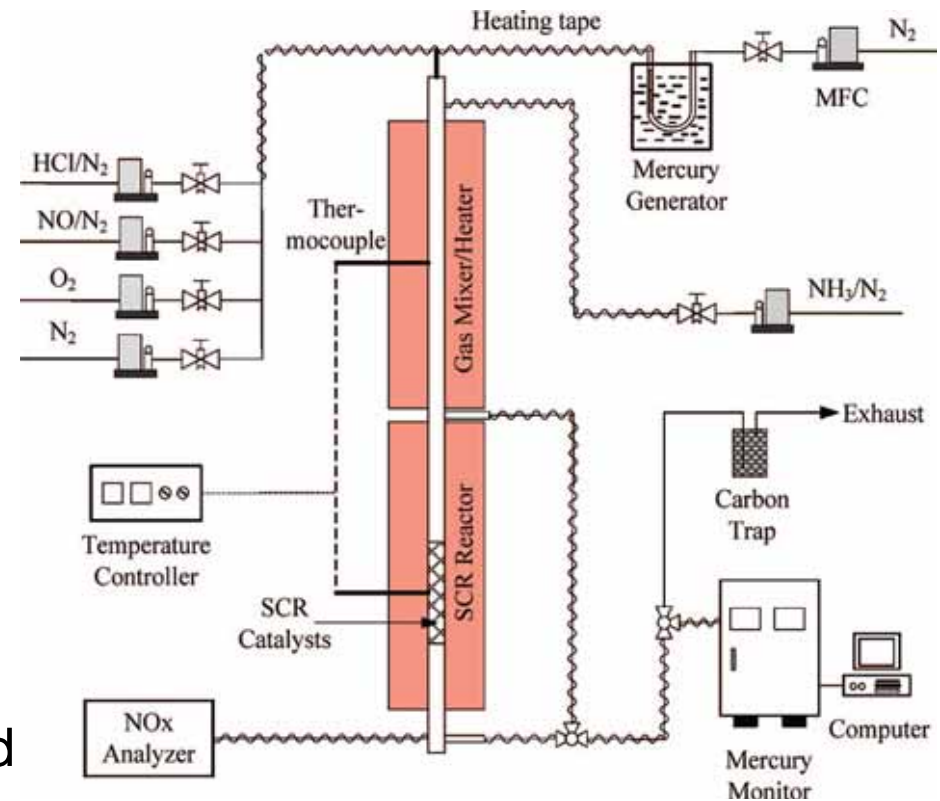
- NO<sub>x</sub> reduction
  - Lab testing can be used to predict field performance
- SO<sub>2</sub> to SO<sub>3</sub> oxidation
  - Lab testing can not be used to predict field performance
    - Fly Ash adsorption of SO<sub>3</sub> in field
    - NH<sub>3</sub> reaction with SO<sub>3</sub> to form ABS
- Hg Oxidation
  - No industry standard lab testing protocol
  - Applicability to field performance still being determined



# Hg Oxidation Lab Testing



- Often volume to area scaling issues
- Potential use
  - Parametric studies
  - Catalyst screening
  - Catalyst surveillance
  - Guarantee testing
- Matching ammonia profile along catalyst length is very important with regards to correlating to field results



Representative Lab schematic

Source: He et al. (2009)



# Relationship between AV, LV and Ammonia Profile



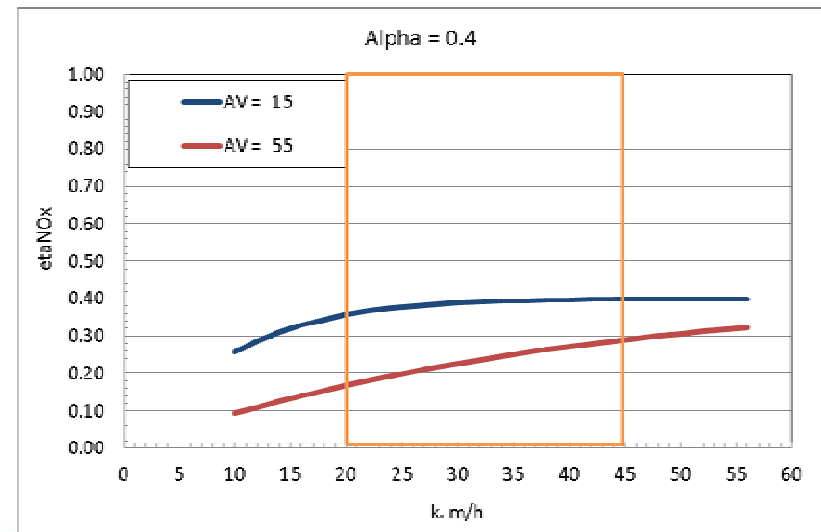
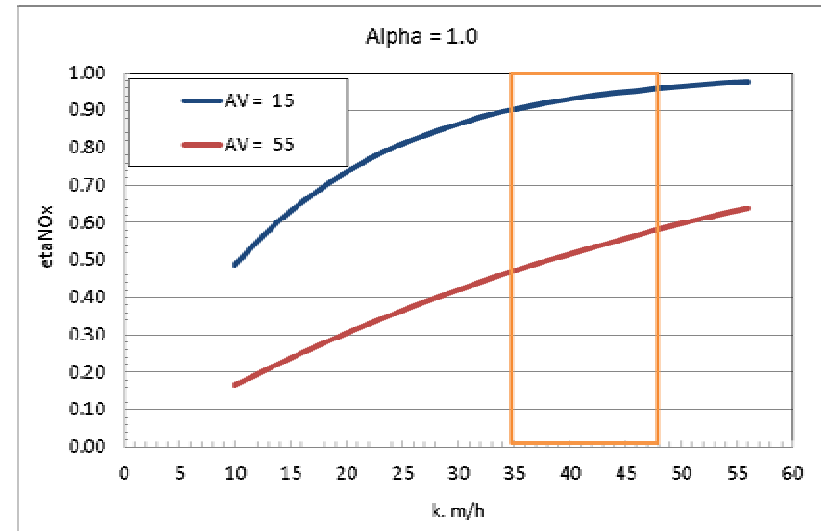
- Matching the ammonia profile in lab reactors can be difficult
  - Full layer area velocity (residence time) and linear velocity can not always be matched simultaneously
  - NO<sub>x</sub> activity dependent on linear velocity, not area velocity
  - Ammonia Profile dependent on area velocity
- Desired to have boundary conditions (inlet NH<sub>3</sub> concentration and outlet NH<sub>3</sub> concentration) as close to field as possible



# Relationship between AV, LV and Ammonia Profile



- At lower AV, outlet NH<sub>3</sub> is less dependent on NO<sub>x</sub> activity
- At lower NH<sub>3</sub>/NO<sub>x</sub> inlet, outlet concentration is approximately constant over expected activity range
- One potential method to approximating ammonia profile may be to match field AV and NH<sub>3</sub>/NO<sub>x</sub>
  - Absolute ammonia and NO<sub>x</sub> concentration should be representative of what catalyst will be seeing



Variables exist in field testing that are not seen in lab testing

- Fuel variations
- Fly ash effects and plugging effects
- Ammonia injection transients
- Minute constituents (other halogens)
- Testing between layers is difficult or impossible (reloads)
- Scales of lab testing and field testing are different
- Large measurement errors



# Takeaways



- Mercury Oxidation over the SCR based on many conditions
- Mercury Oxidation can be transient – not only over the SCR but through the entire system
  - Age effects
  - Boiler/Fuel effects
  - Flow, Temperature, Flue gas variations
- NOx reaction and Hg reaction compete
- Mercury oxidation over SCR for some plants will naturally be very good, other plants may have to enhance mercury oxidation or use alternate mercury capture methods
- Lab testing protocol and subsequent correlation to field performance are not currently available



# Thank You!



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